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THEORETICAL CONSIDERATION OF PLASMA ENERGY TRANSFER TO THE ROCK MASS

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ТЕОРЕТИЧНЕ ОБГРУНТУВАННЯ ПЕРЕДАЧІ ЕНЕРГІЇ ПЛАЗМИ В ГІРСЬКИЙ МАСИВ

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ТЕОРЕТИЧЕСКОЕ ОБОСНОВАНИЕ ПЕРЕДАЧИ ЭНЕРГИИ ПЛАЗМЫ В ГОРНЫЙ МАССИВ

Abstract. The article is devoted to the problem of hard ores, in particular of ferruginous quartzites, thermodynamic destruction with the help of new environmentally friendly and saving-resource technologies of blasting operations in the Kryvyi Rih basin. Until now, no more effective methods have been developed for making underground chambers for explosive substances, than the plasma method, though control of plasma torch thermodynamics remains a live problem. This method allows making chambers of any configurations. The article presents results of theoretical studies of how plasma impacts on the iron ore mass. The dependencies of distribution of temperature loads and normal and tangential stresses in the rock on time and coordinate are specified. It is stated that tensile stresses of magnetic quartzites being treated by plasma is ten times greater than compressive stresses. Calculations, which take into account rock pressure, convective and radiant heat transfer from the plasma jet specify essentially more exactly geometry of stress distribution, time of stress diffusion,

density of thermal field in the surface sector of the borehole. Scientific novelty of the presented results lies in justification of models of plasma-flow impact on the iron ore mass in the pre-fracture zone at the borehole expansion. The results can be used in technological processes of breaking hard ores into the camera, during sinking the raise workings and during construction of the cutting slots and other workings for domestic purposes.

Keywords: chamber cavity, plasma, temperature loads, tensions.

Introduction

At the turn of the twenty-first century low-temperature plasma has shown itself as an important element of the new industrial technologies. Plasma technology allowed us to implement processes, not occurring in the usual classical conditions. The simplest way to obtain plasma is in thermal ionization in electric discharge. The plasma temperature of monatomic gases does not exceed 13000°K , diatomic – 8000°K .

Due to the high temperature and electrical conductivity, plasma has an extremely powerful energetic impact on the treated material, in its role as a universal coolant and reactant. Using plasma can be performed practically any exothermic reaction [1].

Over the last 30-35 years in various industries around the world, the wide application of plasma technology have been found – hardening the surface layer of the products [2], welding and cutting of metals [3], the processing of superhard materials [4, 5], coating [6], the burning of low-grade coals [7].

After a period of formation and development, plasmotron engineering has become an independent branch. Scientific researches in the field of gas dynamics and electrophysics, study of the principles of the plasma torch operation, the interaction of the electric arc with the gas flow, as well as the search for new design schemes and technical solutions have no borders [8].

Problem and communication with scientific and practical tasks

The practice of underground mining of magnetite quartzite in Kryvyi Rih basin have shown the complexity of drilling and blasting complex of works at breaking strong ores. Preparation of cavities for placement of explosives in the rock mass is an important technological component during the roadway. The energy blast emitted by the rock mass of strong ores transforms using the chamber cavity in comparison with the explosion of the cylindrical charge. Nowadays it is possible to create the chamber cavity thermally method using plasma generators. Plasmatrons as a working part on mining machines have found their applications in technologies for mining and ore production, as the breaking of strong ores to the camera, sinking raising and horizontal workings, the creation of cutting slots, draw holes, and other workings for household purposes. Theoretical estimation the changing of the explosion energy, that was emitted in the rock mass during creation a chamber extensions in borehole previously drilled by mechanical means is given in paper [9].

After a period of formation and development of plasma technologies in mining enterprises of Kryvyi Rih basin, needed to produce analytical studies of stress fields in iron ore extended rock mass around the borehole.

A stress state of the rock mass, conditioned by pressure in rocks, affects essentially on process of rock destruction by means of thermal method in technology of the underground borehole reaming. The efficiency of this process is determined by the

nature of thermoelastic stresses distribution, originating in surface layer of borehole. To estimate it and to select the operating conditions of the plasma generator was solved a problem by definition of temperature fields and thermoelastic stresses in borehole walls with allowance for thermal (radiant and convective) and mechanical (forces of a rock pressure) affecting.

Formulation and solution a problem

To determine a field temperature and elastic stresses and their time dependence outside of area, restricted walls of a cylindrical section cavity with radius $r=R$ (fig. 1), inside which one constant temperature T_0 is maintained. The cylindrical surface is exposed to radiant and convective affecting. At the initial moment temperature on a wall equals to zero degrees. Temperature on infinity equals to zero degrees.

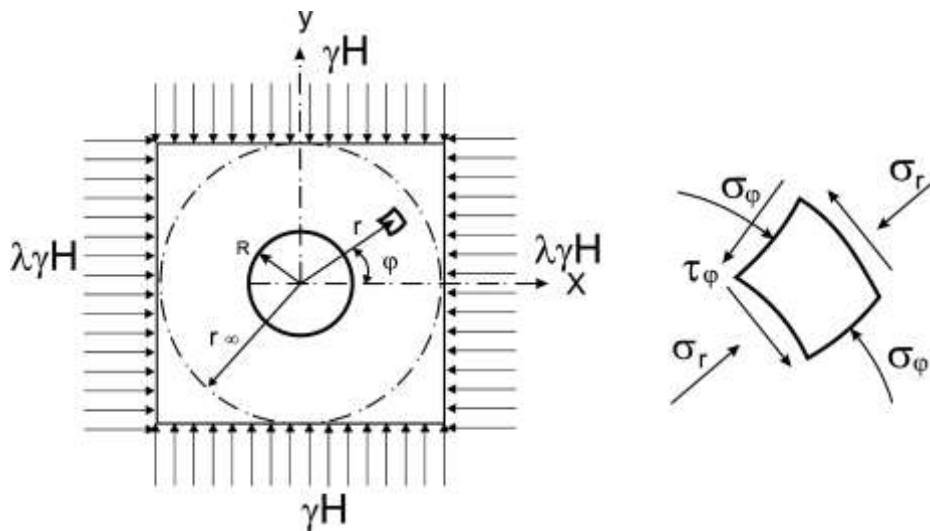


Figure1 – Transverse section of borehole and fragment of the rock mass with the distribution of tensions

It is necessary to solve two differential equations:

$$\frac{\partial^2 T(r,t)}{\partial r^2} + \frac{1}{r} \frac{\partial T(r,t)}{\partial r} = \frac{1}{a} \frac{\partial T(r,t)}{\partial t}$$

$$-\lambda \frac{\partial T(R,t)}{\partial r} = H(T_0 - T(R,t)) + \sigma_0 (T_0^4 - T^4(R,t)),$$

according to following initial and boundary conditions:

$$T(r, t = 0) = 0; T(r = \infty, t) = 0.$$

In this equations a – thermal diffusivity coefficient, λ – thermal conductivity coefficient, H – heat transfer coefficient, σ_0 – Stefan-Boltzmann constant.

Solving a problem, the nonlinear boundary conditions are reduced to a linear dis-

turbance method, then the solution is represented in the way of series with rising degrees and the problem is disintegrated on a sequence of boundary-value problems. After that the method of an integral Laplace transformation will be used and the field of solution is applied to a closed contour due to the functions of a complex variable. After integrating, having taken advantage asymptotic disintegrating of the Bessel functions, the final solution for thermal affecting is obtained.

For definition of a stress tensor around of bore hole with round cross-section in a homogeneous isotropic elastic massif with allowance of thermal affecting and forces of a rock pressure we use a polar coordinate system with the beginning at center of hole. To determine three stress tensor components σ_r , σ_φ , $\tau_{r\varphi}$ and three strain tensor components ε_r , ε_φ , $\varepsilon_{r\varphi}$, is necessary to decide a set of equations, including two equilibrium equations:

$$\frac{\partial \sigma_r}{\partial r} + \frac{1}{r} \frac{\partial \tau_{r\varphi}}{\partial \varphi} + \frac{\sigma_r - \sigma_\varphi}{r} = 0, \quad \frac{\partial \tau_{r\varphi}}{\partial r} + \frac{1}{r} \frac{\partial \sigma_\varphi}{\partial \varphi} + \frac{2\tau_{r\varphi}}{r} = 0,$$

the equation of strain compatibility:

$$\frac{\partial^2 (r\varepsilon_\varphi)}{\partial r^2} - 2 \frac{\partial^2 (r\varepsilon_{r\varphi})}{\partial r \partial \varphi} - r \frac{\partial \varepsilon_r}{\partial r} = 0$$

and three equations, depicting a Hooke law with allowance of thermal expansion:

$$\begin{aligned} \varepsilon_r &= \frac{1+\mu}{E} ((1-\mu)\sigma_r - \mu\sigma_\varphi) + (1+\mu)\beta T \\ \varepsilon_\varphi &= \frac{1+\mu}{E} ((1-\mu)\sigma_\varphi - \mu\sigma_r) + (1+\mu)\beta T \\ \varepsilon_{r\varphi} &= \frac{1+\mu}{E} \tau_{r\varphi}. \end{aligned}$$

In these equations μ – Poisson's ratio, E – isothermal modulus of elasticity, β – linear thermal expansion coefficient, T – function, obtained as a result of a solution of the first part of the problem.

As boundary conditions we take into consideration: with removal from the hole stresses aim to those values, which one act in an undisturbed massif. It was comfort to transform them in Cartesian coordinate system:

$$\lim_{r \rightarrow \infty} \sigma_x = -\lambda \gamma H, \quad \lim_{r \rightarrow \infty} \sigma_y = -\gamma H,$$

where γH – characterizes the quantity of a rock pressure, λ – side thrust coefficient.

On the contour of hole, where $r=R$, it is satisfied the condition $\sigma_r = \tau_{r\varphi} = 0$.

For a solution of this set of equations was used the method, which well-known in theory of elasticity, when three stress tensor components express through one required stress function F :

$$\sigma_r = \frac{1}{r} \frac{\partial F}{\partial r} + \frac{1}{r} \frac{\partial^2 F}{\partial \varphi^2}; \quad \sigma_\varphi = \frac{\partial^2 F}{\partial r^2}; \quad \tau_{r\varphi} = -\frac{\partial}{\partial r} \left(\frac{1}{r} \cdot \frac{\partial F}{\partial \varphi} \right)$$

Having substituted last three expressions in the equations, depicting a Hooke law, and obtained values ε_r and ε_φ in the equation of strain compatibility, finally we shall receive a partial equation for function F :

$$\nabla^2 \nabla^2 F(r, \varphi, t) + \frac{\beta E}{1 - \mu} \nabla^2 T(r, t) = 0, \quad \text{где } \nabla^2 = \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \varphi^2}$$

The general solution is represented in the way of sum of general solutions of a bi-harmonic equation and particular solution of original equation.

Results

The example of calculation of a thermal field for initial temperature $T_0 = 1500$ °C is reduced in a fig. 2.

In fig. 3 are shown consequently dynamics of variation of values a stress tensor components σ_r and σ_φ for initial temperature $T_0 = 1500$ °C at a different valid time of this temperature.

In fig. 4 are shown the stress distribution in a near-surface layer of borehole during plasma exposure for different depth.

Conclusions and recommendations

The solution algorithm of the problem about distribution of temperature and dynamic stresses in mining rocks is developed by means of boreholes expansion by thermal method with allowance for rock pressure and radiant heat change. It is established, that the value of tensile stresses for magnetite quartz in plasma processing is 10 times more than magnitude of compression stresses that confirms the results of the paper [9]. Moreover, the compression stresses are mainly massed in surface heating zone, and tensile stresses are affected further deep into the rock mass. The magnitude of the stresses is influenced by the pressure of rocks. Its contribution may reach 12-17 % in comparison with the values of the stresses in the unstressed rock mass.

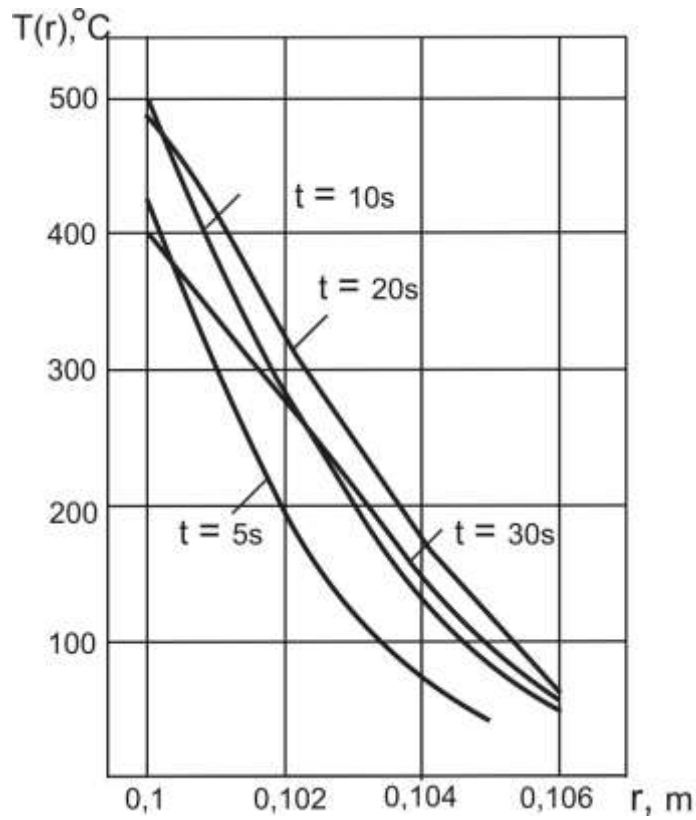


Figure 2 – Distribution of thermal field in a near-surface layer of borehole during plasma exposure

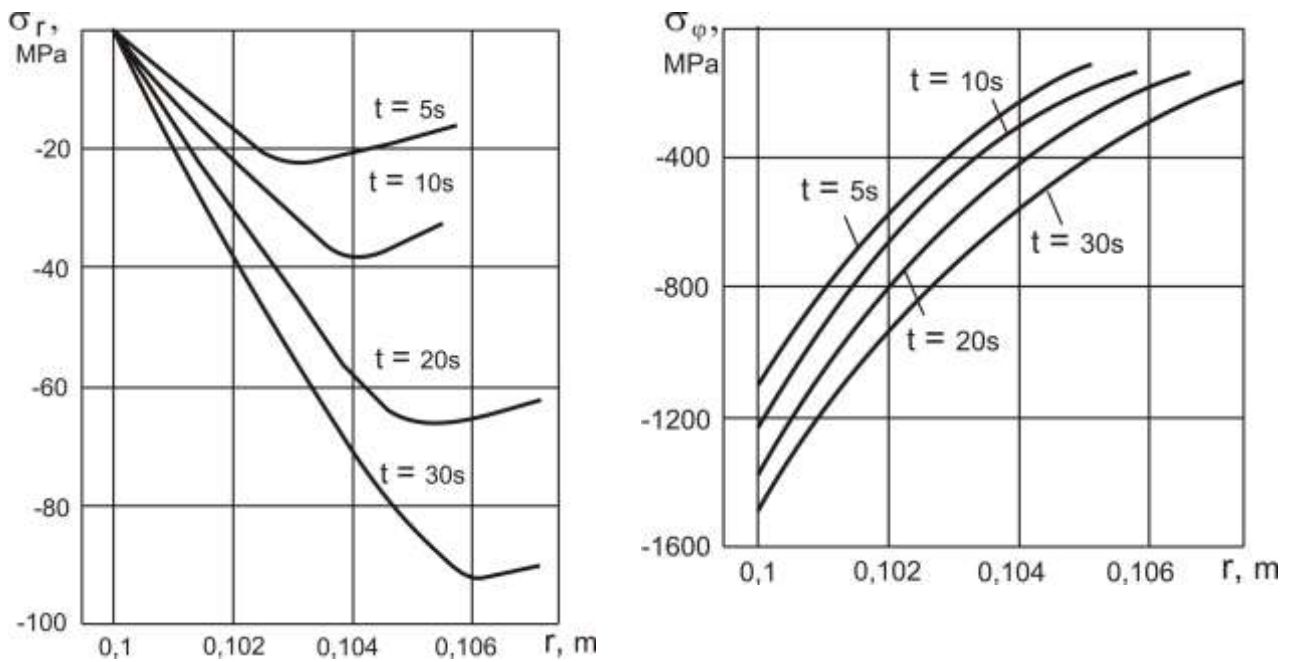
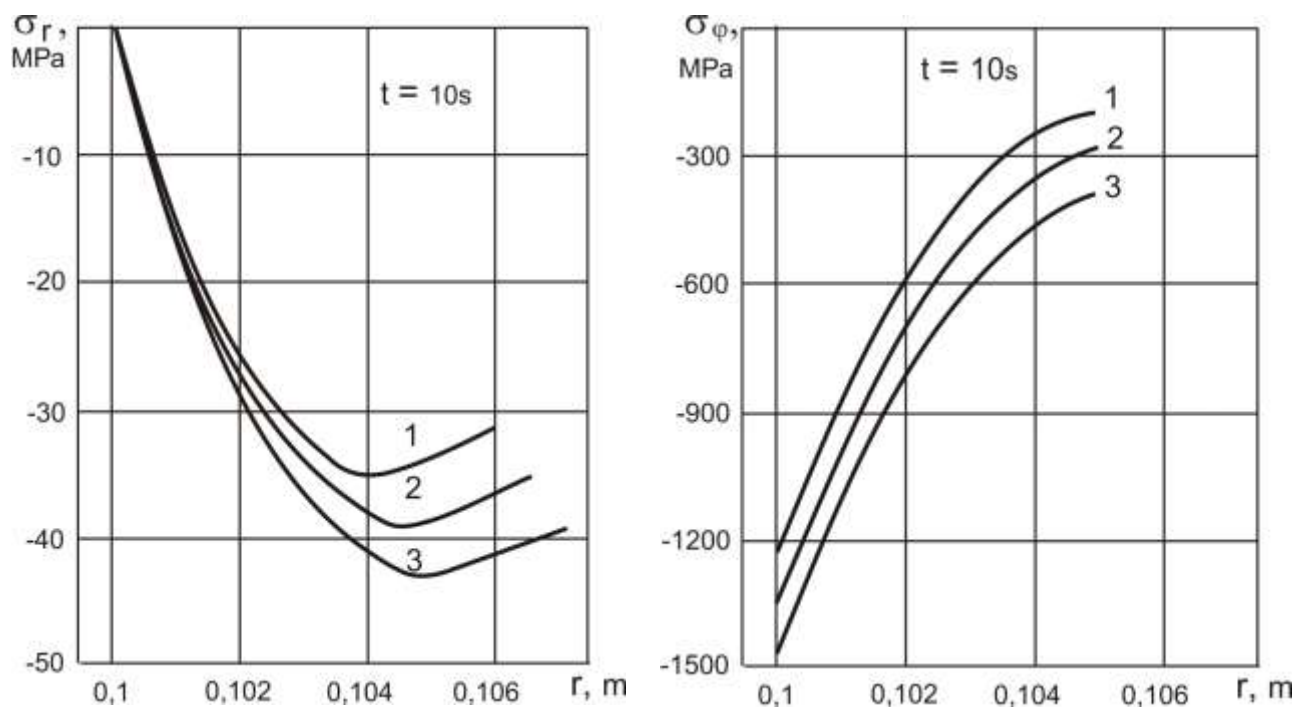


Figure 3 – Stress distribution in a near-surface layer of borehole during plasma exposure



1– $\gamma H = 100$ MPa; 2– $\gamma H = 200$ MPa; 3 – $\gamma H = 300$ MPa
 Figure 4 - Stress distribution in a near-surface layer of borehole during plasma exposure for different depth

The account in calculations of a rock pressure and radiant heat change from the plasma jet has allowed essentially updating geometry of the stress distribution, time of their propagation, density of temperature field in a surface band of borehole. Using the proposed algorithm of solution for each specific geological conditions it is possible to select thermal and structural parameters of the plasma torch ensuring the creation in the rock, the maximum thermal stress and higher productivity of the process of destruction. The obtained results were used in researches of boreholes plasma expansion. The installations have been tested in conditions a series Kryvyi Rih region mines.

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Анотація. Стаття присвячена проблемі термодинамічного руйнування міцних руд, зокрема залістих кварцитів із застосуванням нових екологічних ресурсозберігаючих технологій ведення підривних робіт у Криворізькому басейні. Для підземних умов до теперішнього часу не розроблено більш ефективних методів утворення котлових порожнин для розміщення в них вибухових речовин, ніж плазмовий. Актуальною є проблема управління термодинамікою плазмового факела. Завдяки цьому можна створювати котлові порожнини різних конфігурацій для розміщення вибухових речовин. У статті наведено результати теоретичних досліджень плазмового впливу на залізрудний масив. Отримані залежності розподілу температурного навантаження, нормальних і тангенціальних напружень у гірській породі від часу і по координаті. Встановлено, що величина розтягувальних напружень для магнетитових кварцитів при плазмовій обробці в десять разів більше величини стискуючих напружень. Облік в розрахунках гірського тиску, конвективного і променистого теплообміну від плазмового струменя дозволив істотно уточнити геометрію розподілу напружень, час їх поширення, щільність теплового поля в поверхневій зоні свердловини. Наукова новизна наведених результатів полягає в обґрунтуванні моделей впливу плазмових потоків на залізрудний масив в зоні передруйнування при розширенні свердловини. Наведені результати можуть бути використані в технологічних процесах відбивання міцних руд на камеру, при проходці піднятих виробок, при спорудженні відрізних щілин та інших виробок господарського призначення.

Ключові слова: котлова порожнина, плазма, температурне навантаження, напруження

Аннотация. Статья посвящена проблеме термодинамического разрушения крепких руд, в частности железистых кварцитов с применением новых экологических ресурсосберегающих технологий ведения взрывных работ в Криворожском бассейне. Для подземных условий до настоящего времени не разработано более эффективных методов образования котловых полостей для размещения в нем взрывчатых веществ, чем плазменный. Актуальной является проблема управления термодинамикой плазменного факела. Благодаря этому можно создавать котловые полости различных конфигураций для размещения взрывчатых веществ. В статье приведены результаты теоретических исследований плазменного воздействия на железорудный массив. Получены зависимости распределения температурной нагрузки, нормальных и тангенциальных напряжений в горной породе от времени и по координате. Уста-

новлено, что величина растягивающих напряжений для магнетитовых кварцитов при плазменной обработке в десять раз больше величины сжимающих напряжений. Учет в расчетах горного давления, конвективного и лучистого теплообмена от плазменной струи позволил существенно уточнить геометрию распределения напряжений, время их распространения, плотность теплового поля в поверхностной зоне скважины. Научная новизна приведенных результатов заключается в обосновании моделей воздействия плазменных потоков на железорудный массив в зоне предразрушения при расширении скважины. Приведенные результаты могут быть использованы в технологических процессах отбойки крепких руд на камеру, при проходке восстающих выработок, при сооружении отрезных щелей и других выработок хозяйственного назначения.

Ключевые слова: котловая полость, плазма, температурная нагрузка, напряжения.

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