

PHENOMENOLOGICAL DESCRIPTION OF NEUTRON YIELDS FROM ACTINIDE FISSION

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The phenomenological analysis of the neutron yields from the fission of ^{233}U , ^{235}U , ^{239}Pu and ^{252}Cf has been performed. The parameterization used allows the peculiarities of the 'sawtooth' curve of neutron multiplicity for light and heavy fragments to be described and predicted.

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Studying characteristics of actinide nucleus fission products, such as mass and charge distribution, average number of prompt neutrons and excitation energies of fragments, is essential for understanding basic mechanisms of the fission process [1]. These characteristics are widely used in various application fields, e.g. in nuclear energy, non-destructive analysis, active and passive detection of special nuclear materials in context of their non-proliferation, etc. Information on primary fission fragments (with respect to neutron emission) is necessary for precise theoretical analysis of the experimental data. Direct measuring of primary fragments' properties relative to neutron emission is a complicated task. At the same time knowledge of neutron yield dependence on mass of fission fragments is important for understanding dynamics of the fission process. Variation of average neutron multiplicity pattern reflects change of different fission mode dynamic effects [2]-[4]. Number of emitted neutrons depends on mass number and charge of the nucleus, total excitation energy of fission fragments, redistribution of total excitation energy between light and heavy fragments and angular momenta of primary fission fragments. Therefore to give quantitative description of average multiplicity of fission neutrons [5]-[7] we need multi-parametric experimental data. According to Terrel calculating method system of the integral equations [8],[9].

$$\begin{aligned} \int_0^{A_i - \nu_F(A_i)} Y(A)dA &= \\ &= \int_0^{A_i} y(A)dA + \frac{1}{2} \frac{dy}{dA} <\sigma^2(\nu_F, A)> + \dots, \end{aligned} \quad (1)$$

can be solved only on the basis of experimental data on total fission yields in the final state, $y(A)$ - initial fragment yields with the mass number A before

neutron emission; $\sigma^2(\nu_F, A)$ - variation, ν_F - total neutron yield.

As it was shown in [8] higher-order terms make small contribution. For example, contribution $\frac{1}{2} \frac{dy}{dA} <\sigma^2(\nu_F, A)>$ into $\nu_F(A)$ is less than 0,1. Essence of Terrell calculating method (see Fig.5 [8]) is illustrated in Fig.1, where initial cumulative mass distributions of light and heavy fragments

$$S_y^L = \int_0^{A_L} y(A)dA,$$

$$S_y^H = \int_{A_F - A_L}^{A_F} y(A)dA$$

and final cumulative mass distributions of light and heavy fragments

$$S_Y^L = \int_0^{A_L} Y(A)dA,$$

$$S_Y^H = \int_{A_F - A_L}^{A_F} Y(A)dA$$

are plotted with circles and interpolated curves [10].

Values of total neutron yields $F(A)$ are taken to be the absolute difference between point values and complementary function values, illustrated in Fig.1 by the horizontal line, so that

$$\nu_F(A) = \nu_L(A) + \nu_H(A), \quad (2)$$

where ν_L and ν_H are neutron yields from light and heavy fragments, respectively. To calculate $\nu_{L,H}$ according to (1) it is necessary to set their optimal parameterization type in advance. On one hand, parameterization should contain as few free parameters as

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possible; on the other hand, it should fully reflect expected local peculiarities. For this purpose we employ Wahl parameterization [10] by introducing function

$$R(A) = \nu_{L,H}(A)/\nu_F(A). \quad (3)$$

Generalized shape of $R(A)$ function contains only 2 x 4 segments for both light and heavy fragments (dotted line on Fig.2), which is sufficient for qualitative description of existing experimental data on yields of neutrons emitted by fission fragments (see Fig.4.2.42 [10]).

Our recent analysis [11] of existing experimental data on neutron yields from fragments of ^{252}Cf , ^{244}Cm and ^{248}Cm spontaneous fission [12] has shown that to consider dependence of fission neutron yields on mass more accurately, range of the fragment masses should be divided into more than 4 segments (solid broken line on Fig.2). To find consistent patterns in fission neutrons distribution depending on fragment mass, we have chosen smoothed and normalized empiric values of fission neutrons yields $\nu_{L,H}(A)$ for $^{233}\text{U}(\text{n,f})$, $^{235}\text{U}(\text{n,f})$, $^{239}\text{Pu}(\text{n,f})$ and $^{252}\text{Cf}(\text{s,f})$, obtained in [13], which are in reasonable agreement with the experimental data (see Fig.1 there). $R(A)$ function for light and heavy fragments is parameterized as

$$R_i^L(A) = A_i^L + B_i^L(A - A_L). \quad (4)$$

$$R_i^H(A) = 1 - R_i^L(A_H), \quad (5)$$

where i - segment number, a_i^L , b_i^L - parameters. Value of A_L is determined from condition: $R(A_L) = 0,5$. We calculated $R(A)$ for $^{233}\text{U}(\text{n,f})$, $^{235}\text{U}(\text{n,f})$, $^{239}\text{Pu}(\text{n,f})$ and $^{252}\text{Cf}(\text{s,f})$ fission in accordance with (4) and (5), dividing the whole data range into 6 segments, as it is seen on Fig.2. Taking into account the following relations can substantially decrease number of the free parameters:

$$a_4 = 0,5; b_2 = 0; A_0 = (A_F - 4)/2; \quad (6)$$

$$a_1 + b_1(A_0 - A_L) = 0,5; \quad (7)$$

$$a_1 + b_1(A_1 - A_L) = a_3 + b_3(A_2 - A_L) = a_2; \quad (8)$$

$$a_{i+1} + b_{i+1}(A_{i+1} - A_L) = a_i + b_i(A_i - A_L). \quad (9)$$

Values of parameters a_i and b_i are determined from the calculated $R(A)$ function and relations (6) - (9). Results of the calculation are given on Fig. 3 and Table 1. Shape of $\nu_{L,H}(A)$ can be obtained from (3). As it is seen on Fig. 5, calculated values of fission neutron yields practically everywhere coincide with initial values, obtained by Wahl [13].

Empiric $R(A)$ function possesses number of characteristic features:

- $R(A) = 0,5$ in the point of symmetric fission, which is determined as $A_0 = (A_f - 4)/2$ [13], and also in the point A_L , determined by adjustment;

- maximal value of $R(A)$ function is restricted by 0,83 - 0,90 range;
- number of points at A_1A_2 plateau is 3 - 4 a.m.u.;
- position of A_1 point linearly depends on actinide mass (see Fig. 4.) and is determined from the condition of $R(A)$ function minimum value in the complementary point, corresponding to fission product mass $A_N = 129-130$ a.m.u.;
- value of A_L and parameters a_i , b_i , also obey linear dependence in the probed range of actinide masses;
- A_0A_5 segment is almost constant and slightly varies within 39 - 41 a.m.u. range.

The performed calculation allows to estimate possible values of fission neutron yields from light and heavy fragments based on the known total average yields, which, in its turn, can be obtained only from mass distribution of fission fragments with help of modified Terrell method [8],[9].

Using graph on Fig.3 and the abovementioned regularities we can estimate neutron yields for $^{237}\text{Np}(\text{n,f})$ fission: $A_0 = 117$; $A_L = 94$; $A_1 = 106$; $A_2 = 103$; $A_3 = 97$; $A_4 = 90$; $A_5 = 78$; $R_{max} = 0,9$; $R(A_5) = R(A_6) = 0,2$; $b_3 = 0,05$.

Anticipated behaviour of $R(A)$ function for $^{237}\text{Np}(\text{n,f})$ fission is presented by dotted curve on Fig.3.

In the present paper phenomenological analysis of neutron yields of ^{235}U , ^{235}U , ^{239}Pu and ^{252}Cf fission fragments is performed. Chosen parameterization and established regularities allow to describe observed changes of 'sawtooth' behaviour of fission neutron yields for light and heavy fission fragments.

Using the established regularities (solid curves on Fig.3) behaviour of $R(A)$ function for $^{237}\text{Np}(\text{n,f})$ fission is predicted (dotted curve on Fig.3). It is obvious from Fig.5 that we obtained good quantitative agreement with initial fission neutron yields for the whole range of the fragment masses.

This parameterization can be used for solving integral equations of type (1) to determine fission fragments' yields before neutron emission.

Table 1. Parameters of $R(A)$ function for fission fragments of $^{233}U(n,f)$, $^{235}U(n,f)$, $^{239}Pu(n,f)$ and $^{252}Cf(s,f)$

| ^{252}Cf (s.f) | $A_L=105$ | | | | | |
|---------------------|----------------|----------------|----------------|----------------|----------------|----------------|
| | a ₁ | a ₂ | a ₃ | a ₄ | a ₅ | a ₆ |
| | 2,4 | 0,9 | 0,51 | 0,50 | 0,47 | 0,20 |
| | b ₁ | b ₂ | b ₃ | b ₄ | b ₅ | b ₆ |
| | -0,10 | 0,0 | 0,038 | 0,020 | 0,013 | 0,0 |
| | A ₀ | A ₁ | A ₂ | A ₃ | A ₄ | A ₅ |
| | 124 | 120 | 117 | 107 | 100 | 83 |

| ^{239}Pu (n,f) | $A_L=95$ | | | | | |
|---------------------|----------------|----------------|----------------|----------------|----------------|----------------|
| | a ₁ | a ₂ | a ₃ | a ₄ | a ₅ | a ₆ |
| | 1,4 | 0,83 | 0,32 | 0,50 | 0,49 | 0,20 |
| | b ₁ | b ₂ | b ₃ | b ₄ | b ₅ | b ₆ |
| | -0,04 | 0,0 | 0,050 | 0,006 | 0,016 | 0,0 |
| | A ₀ | A ₁ | A ₂ | A ₃ | A ₄ | A ₅ |
| | 118 | 110 | 105 | 100 | 94 | 88 |

| ^{235}U (n,f) | $A_L=92$ | | | | | |
|--------------------|----------------|----------------|----------------|----------------|----------------|----------------|
| | a ₁ | a ₂ | a ₃ | a ₄ | a ₅ | a ₆ |
| | 1,2 | 0,85 | 0,42 | 0,50 | 0,50 | 0,20 |
| | b ₁ | b ₂ | b ₃ | b ₄ | b ₅ | b ₆ |
| | -0,03 | 0,0 | 0,050 | 0,020 | 0,021 | 0,0 |
| | A ₀ | A ₁ | A ₂ | A ₃ | A ₄ | A ₅ |
| | 124 | 104 | 101 | 97 | 86 | 77 |

| ^{233}U (n,f) | $A_L=90$ | | | | | |
|--------------------|----------------|----------------|----------------|----------------|----------------|----------------|
| | a ₁ | a ₂ | a ₃ | a ₄ | a ₅ | a ₆ |
| | 1,2 | 0,85 | 0,35 | 0,50 | 0,55 | 0,20 |
| | b ₁ | b ₂ | b ₃ | b ₄ | b ₅ | b ₆ |
| | -0,03 | 0,0 | 0,050 | 0,020 | 0,025 | 0,0 |
| | A ₀ | A ₁ | A ₂ | A ₃ | A ₄ | A ₅ |
| | 115 | 102 | 99 | 85 | 840 | 76 |

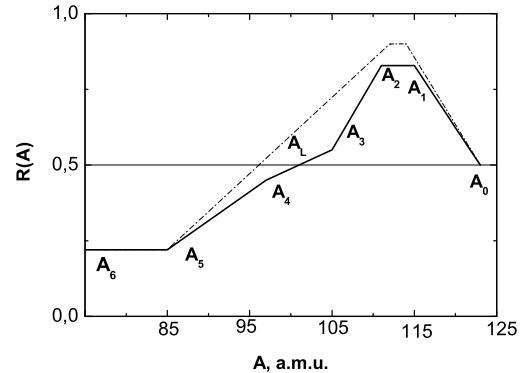


Fig.2. $R(A)$ - functions. Solid line represents our parameterisation; dotted curve is Wahl parameterization [10]

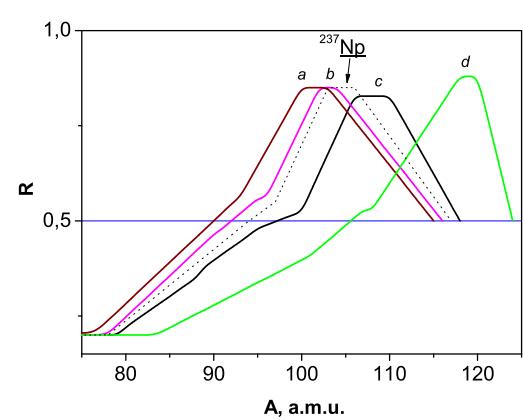


Fig.3. Calculated $R(A)$ for fission of a) $^{233}U(n,f)$, b) $^{235}U(n,f)$, c) $^{239}Pu(n,f)$, d) $^{252}Cf(s,f)$; and predicted $R(A)$ for $^{237}Np(n,f)$ fission reaction (dotted line)

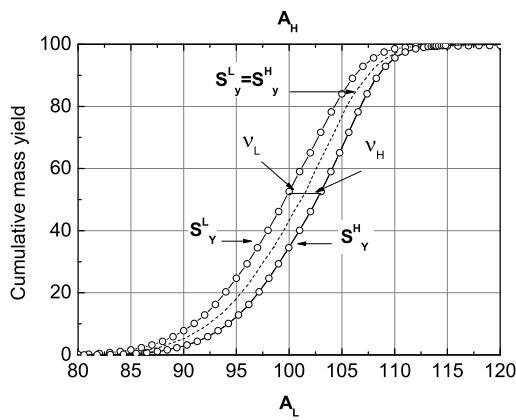


Fig.1. Typical curves of cumulative mass yields S_y^L , S_y^H , S_y^L and S_y^L used to find neutron yields v_L , v_H depending on mass of fission fragments

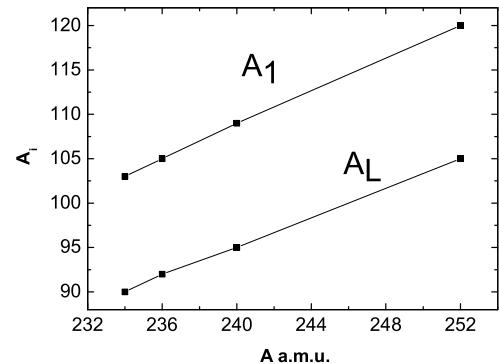


Fig.4. Behavior of the outermost points of $R(A)$ segments

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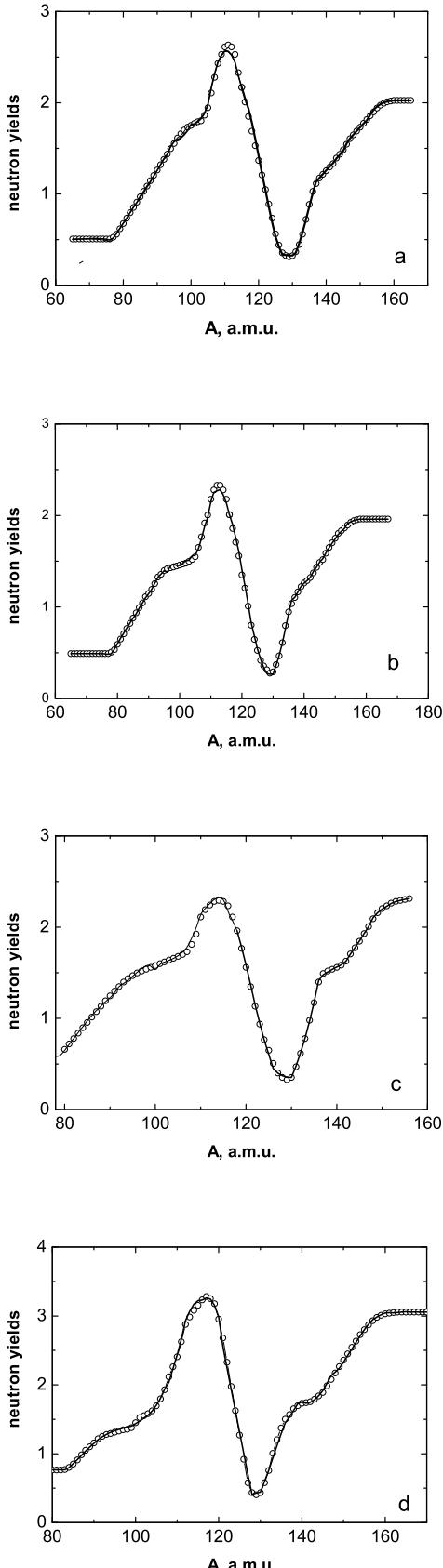


Fig.5. Fission neutron yields $\nu_{L,H}(A)$ for light and heavy fragments: a) $^{233}\text{U}(n,f)$, b) $^{235}\text{U}(n,f)$, c) $^{239}\text{Pu}(n,f)$, d) $^{252}\text{Cf}(s.f.)$; solid curve is the result of $\nu_{L,H}(A)$ calculation; circles are smoothed and normalized values of fission neutron yields [13]

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ФЕНОМЕНОЛОГИЧЕСКОЕ ОПИСАНИЕ ВЫХОДОВ НЕЙТРОНОВ ДЕЛЕНИЯ АКТИНИДОВ

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Проведен феноменологічний аналіз виходів нейtronів з уламків делення ^{233}U , ^{235}U , ^{239}Pu і ^{252}Cf . Вибрана параметризація і установлені закономірності дозволяють описати і предсказувати наблюдаемі зміни "пилообразного" поведінки виходу нейtronів з легкого та важкого уламків делення ядер.

ФЕНОМЕНОЛОГІЧНИЙ ОПИС ВИХОДІВ НЕЙТРОНІВ ПОДІЛУ АКТИНІДІВ

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Виконано феноменологічний аналіз виходів нейtronів з уламків поділу ^{233}U , ^{235}U , ^{239}Pu та ^{252}Cf . Вибрана параметризація та встановлені закономірності дозволяють описати та передбачити зміни "пилоподібної" поведінки виходу нейtronів з легкого та важкого уламків поділу ядер, які спостерігаються.