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Preparation of Co–Gr Nanocomposites and Analysis of Their Tribological and Corrosion Characteristics

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This work summarizes the tribological and corrosion behaviour of Co–Gr nanocomposites. The Co–Gr nanocomposites are synthesized using highenergy ball mill and compacted into cylindrical pellets by hydraulic pressing. The composites are characterized using SEM, EDAX, and AFM. The dry sliding wear results reveal that the wear resistance increases with increase in the percentage of graphite (Gr). The corrosion characteristics of the Co–Gr nanocomposites are examined using immersion and electrochemical methods. The electrochemical polarization results reveal the increase in corrosion resistant of the Co–25Gr nanocomposites ($E_{\rm corr} = -0.416$ V vs Ag/AgCl) to more positive side than pure Co (-0.443 V). Electrochemical impedance spectroscopy analysis results also confirmed Co–25Gr nanocomposite has higher resistance value (100 Ω). The results of the weight loss method also authenticate increase in corrosion resistance of Co–25Gr nanocomposite.

Key words: wear, corrosion, EDAX, SEM, AFM.

У роботі представлено узагальнюючі результати досліджень трибологічної та корозійної поведінки нанокомпозитів Co–Gr. Нанокомпозити Co– Gr було синтезовано з використанням високоенергетичного кульового млина та скомпактовано у циліндричні ґранули шляхом гідравлічного пресування. Композити досліджено за допомогою СЕМ, ЕДС та АСМ. Показано, що в результаті сухого ковзання опір зношуванню зростає зі збі-

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льшенням процентного вмісту графіту (Gr). Також досліджено корозійні характеристики нанокомпозитів Co-Gr з використанням імерсійних та електрохемічних метод. Результати електрохемічної поляризації показали підвищення корозійної стійкости нанокомпозитів Co-25Gr ($E_{\rm corr} = -0,416$ В у зіставленні з Ag/AgCl); значення відповідного потенціялу зміщене у позитивному напрямку відносно чистого Co (-0,443 B). Результати аналізи електрохемічної імпедансної спектроскопії також підтвердили, що нанокомпозит Co-25Gr має вище значення електроопору (100 Ом). Результати, одержані методою визначення втрати ваги, також підтвердили зростання корозійної стійкости нанокомпозиту Co-25Gr.

Ключові слова: знос, корозія, ЕДС, СЕМ, АСМ.

В работе представлены обобщающие результаты исследования трибологического и коррозионного поведения нанокомпозитов Co-Gr. Нанокомпозиты Co-Gr были синтезированы с использованием высокоэнергетической шаровой мельницы и скомпактированы в цилиндрические гранулы путём гидравлического прессования. Композиты были исследованы с помощью СЭМ, ЭДС и АСМ. Показано, что в результате сухого скольжения сопротивление износу возрастает с увеличением процентного содержания графита (Gr). Также исследованы коррозионные характеристики нанокомпозитов Co-Gr с использованием иммерсионных и электрохимических методов. Результаты электрохимической поляризации показали увеличение коррозионной устойчивости нанокомпозитов Co-25Gr $(E_{\rm corr} = -0,416$ В в сопоставлении с Ag/AgCl); значение соответствующего потенциала смещено в положительном направлении относительно чистого Со (-0,443 В). Результаты анализа электрохимической импедансной спектроскопии также подтвердили, что нанокомпозит Co-25Gr имеет более высокое значение электросопротивления (100 Ом). Результаты, полученные методом определения потери веса, также подтвердили увеличение коррозионной стойкости нанокомпозита Co-25Gr.

Ключевые слова: износ, коррозия, ЭДС, СЭМ, АСМ.

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1. INTRODUCTION

The materials used for dental prostheses and orthopaedic implants should have high corrosion resistance, wear resistance and high mechanical strength. The cobalt is such kind of material, which is basically used in orthopaedic and dental applications because of their improved resistances together with formability [1, 2].

The dental implants are of two different types such as permanent or removable framework structures [3]. In order to improve the corrosion and wear resistance of cobalt, Cr, Ni and Mo are normally added as reinforcement [4, 5]. However, the addition of these materials not only improves the strength and properties of alloy but also increases the toxicity, which in turn has an adverse effect [6].

Graphite reinforced composites are a potential replacement for materials such as Cr, Mo, *etc.* [7]. Graphite is a biodegradable and biocompatible material with good physical and mechanical properties [8, 9]. The mechanical and physical properties of bulk composites can be further improved by reinforcement of nanoparticle with base materials [10, 11].

Although there are a few previous studies focused on mechanical and tribological properties of Co-based alloys [3], the study on the effect of reinforcement of nanographite in cobalt matrix is unexplored up to the author's knowledge.

In this study, the Co–Gr nanocomposites are fabricated by a combination of powder metallurgy and hydraulic pressing process. The composites are obtained in various proportions. The dry sliding wear and electrochemical corrosion characteristics of the composites are studied in detail. The results of the studies are expected to substantiate the application of Co-graphite nanocomposites in dental and orthopaedic implants.

2. MATERIALS and METHODS

2.1. Materials and Preparation of Composite Materials

The Co and Gr powders used in this work were of research grade having a purity level of 99.5% and 99% respectively. The nanographite powders were synthesized using high-energy ball mill (Fritsch pulverisette, Germany), 40 g of graphite powder and nearly 800 g of WC (50 balls). The powder to ball weight ratio was maintained at 1:20 and the ball milling process was carried out for 5 h in order to achieve nanographite. The Co–Gr nanocomposites of different weight proportions (95:05, 90:10, 85:15, 80:20, and 75:25) were prepared by mixing in a high-energy ball mill. The composite powder was then directly fed into a cylindrical die of 8 mm diameter and 50 mm height and compacted into a cylindrical pellet of height 20 mm by applying a load of 0.5 GPa in a hydraulic press and sintered at the temperature of 600° C for 1 hour in order to harden the green compact into composite pellets.

2.2. Characterization

The surface topography of Co–Gr nanocomposites was studied using Atomic Force Microscopy (XE70, Park System, South Korea) in a noncontact mode using a Si_3N_4 tip having a radius of curvature of less than 10 mm. The scan size and constant are 10×10 µm and 40 N/m respectively. The morphological characterization of the composite was done using SEM (Hitachi SU1510, Secondary Electron Mode, 10 kV, the emission current of 96 µA). The compositional analysis was studied using EDX (QUANTAX–Bruker).

2.3. Pin on Disc Dry Sliding Wear Test

The Co-Gr nanocomposite pellets of 8 mm diameter and length of 20 mm are used as the test sample. The test was done using pin on disc apparatus (DUCOM, Bangalore) according to ASTM: G99 standards. The disc selected for the experiment was EN31 steel. The composite sample and the disc were cleaned to remove impurities using acetone before the test starts. The wear test was carried out at various load ranges such as 5, 10, 15, and 20 N and at varying sliding distant from 500 m to 2000 m [8]. The sliding speed is also varied from 0.5 m/s to 2 m/s. The initial and final weights of the composite specimens were measured using an electronic weighing scale so as to determine the weight loss of the specimens [12, 13].

2.4. Potentiometric Polarization Test

The potentiometric polarization test was used to investigate the electrochemical corrosion behaviour of Co-Gr nanocomposites. The potentiometric tests were studied using Biologic SP-150 potentiostat controlled using the EC-Lab®software. The experiments were performed using three electrode cell consists of platinum wire counter electrode Ag/AgCl reference electrode and the Co–Gr nanocomposite pellet as a working electrode. The polarization tests were carried out at 25°C with the 1 N H_2SO_4 solution. The composite pellets were polished with emery paper and rinsed with acetone and double distilled water prior to the electrochemical tests. The Co-Gr nanocomposite pellets, which were used as working electrode, were immersed in the electrolyte solution of 1 N H₂SO₄ for 1 h. in order to reach steady state condition, and the OCP was measured. The potentiometric polarization curves were obtained at the scan rate of $5 \,\mathrm{mV/s}$. The corrosion potential $E_{\rm corr}$ and current density $I_{\rm corr}$ were obtained using EC lab software through Tafel fit extrapolation [4, 14, 15].

2.5. Electrochemical Impedance Spectroscopy

The electrochemical impedance spectroscopy (EIS) for the composites was performed at the range of 100 kHz to 100 MHz and the initial sinusoidal voltage signal was 10 mV. The experiments were carried out using Biologic SP-150 electrochemical workstation against open circuit potential. The EIS data were then fitted and analysed using the EC-lab software [14, 16–18].

2.6. Immersion Test

The weight loss of the Co-Gr nanocomposite in the various corrosive

mediums was studied, and the percentage of weight loss is calculated. The corrosive medium such as 0.1 N and 0.5 N HCl, H_2SO_4 and 10% NaCl were used for this purpose. The Co–Gr nanocomposite pellets are immersed in each of the above-mentioned electrolytic solutions for 24 h. After that, the samples were removed from the solutions, washed with distilled water, and dried at room temperature, and the changes in weight of the composites were used to calculate the percentage weight loss [19].

3. RESULTS AND DISCUSSION

3.1. SEM Analysis

Figure 1, a and b shows the surface morphology and EDAX spectrum of Co–Gr nanocomposites. The SEM image clearly reveals the homogeneous mixture of Co–Gr nanocomposites. The EDAX spectrum confirms the presence of cobalt and graphite in the composite material. The particle size of Co and Gr were found to be in the range of 10 microns and 80-150 nm respectively. The Gr nanoparticles were found to be agglomerated.

Figure 2 shows the surface morphology of Co–Gr composite pellets before the test, which shows the uniform dispersion of Gr in Co–matrix.

Figure 3, *a* and *b* reveals the worn out surfaces of the pure Co and



Fig. 1. SEM image (*a*) and EDAX spectrum (*b*) of Co–Gr nanocomposite.



Fig. 2. SEM micrograph of Co-25Gr nanocomposite pellets before wear test.



Fig. 3. SEM micrograph of pure Co (a) and Co-25Gr nanocomposite (b) pellets after wear test.

composite pellets after sliding wear test. The scratches and grooves were formed in the direction of sliding which confirms the mechanism of wear due to abrasive wear between the composite pellet and rotating disc. The SEM micrograph shows very less change in the subsurface microstructure of the Co–Gr pellets as compared to pure Co, which attributes to the improved wear resistance because of nanographite reinforcement.

3.2. AFM Analysis

Surface topography of the composite materials was evaluated using



Fig. 4. 3D AFM image of Co-25Gr nanocomposite.



Fig. 5. 2D AFM image (a), line profile analysis (b) and histogram (c) of Co-25Gr nanocomposite.

AFM.

Figure 4, the 3D AFM image shows the height and width of the composite materials which is found to be around 10-20 nm and 500 nm respectively. Figure 5, a-c are 2D AFM image and its corresponding line diagram and histogram. The AFM 2D analysis also confirms that the particle height is in the range of 10-20 nm.

3.3. Sliding Wear Analysis

The wear analysis is done using pin-on-disc apparatus for the study of tribological characteristics of novel Co–Gr nanocomposites. From Figure 6, we can learn that the addition of Gr nanoparticles decreases the



Fig. 6. Wear loss of Co and Co–Gr nanocomposite: applied load (*a*), sliding distance (*b*), sliding speed (*c*).

wear loss of the composites as compared to that of pure Co pins. The results reveal that increase in the percentage of nanographite in Comatrix has further increased the wear resistance. The Co-25Gr nanocomposites have lesser wear loss than Co-5Gr. Figure 6, *a* shows the wear loss incurred by specimens at various loads ranging from 5 N to 20 N. From the graphs, it is evident that the Co-Gr composites have higher wear resistance at different loads but the wear loss increases with increase in load, this may be due to softening of composites due to increase in temperature at the interface. The wear loss phenomenon ranging from 500 m to 2000 m is shown in Fig. 6, *b*. It can be noted that increase in Gr in nanocomposites decreases the wear loss, which may be due to the lubricating effect of nanographite reinforcements. Figure 6, *c* represents the trend of wear loss of composite materials at various sliding speed. From this figure, it is clear that the wear loss decreases with increase in sliding speed.

3.4. Coefficient of Friction Analysis (COF)

Figure 7 shows the various trends of coefficient of friction of Co-Gr



Fig. 7. COF of Co and Co–Gr nanocomposite: applied load (*a*), sliding distance (*b*), sliding speed (*c*).

nanocomposites. The COF decreases with increase in nanographite content; this is because of the lubricating property of nanographite particles, which improves the self-lubricating capacity of the composites.

The results utter that the COF of Co–25Gr nanocomposite is lower compared to that of pure cobalt pellet. The coefficient of friction of composite specimens is shown in Fig. 7, a, which reveals that the COF of the pure cobalt and composite pellets increases with an increase in load.

From Figure 7, b, it is evident that the COF values of pure Co and Co–Gr nanocomposites are relatively low when the sliding distance is less and the COF further increases with an increase in sliding distance. The evaluation of Fig. 7, c dictates there is a linear decrement in COF values with increase in sliding speed.

3.5. Potentiometric Polarization Analysis

The potentiometric polarization analyses of the pure cobalt and various compositions of Co–Gr nanocomposites in 5% wt. NaCl solution is plotted in Fig. 8; the graphs are plotted against potential voltage and current density. The composite materials show stable passive region



Fig. 8. Potentiometric polarization curves of Co and Co-Gr nanocomposites.

No	Specimen	$E_{\rm corr}$, V	$I_{ m corr} \cdot 10^{-3}$, $\mu A/ m cm^2$	Polarization resistance R_p , $\Omega \cdot \mathrm{cm}^2$
1	Pure Co	-0.443	8.528	1.06
2	Co-5Gr	-0.437	5.933	4.35
3	Co-10Gr	-0.436	5.910	4.41
4	Co-15Gr	-0.435	4.912	5.31
5	Co-20Gr	-0.419	2.425	9.89
6	Co-25Gr	-0.416	1.767	14.8

TABLE 1. Corrosion characteristics of the pure Co and Co-Gr nanocomposites.

after -0.6 V. The current density remains more or less constant with increase in potential voltage. This phenomenon is due to the formation of oxide layers at the surface of the specimen.

The corrosion characteristics such as corrosion potential $(E_{\rm corr})$, current density $(I_{\rm corr})$ and polarization resistance (R_P) are determined by Tafel extrapolation method. From Table 1, it can be understand that corrosion potential $(E_{\rm corr})$ of Co-25Gr nanocomposites (-0.416 V vs Ag/AgCl) is increased than that of pure Co (-0.443 V vs Ag/AgCl), which confirms the increase in corrosion resistance of the composites. The current density of the Co-25Gr nanocomposites (1.767 \cdot 10^{-3} \mu A/cm²) has reduced considerably when compared to pure Co (8.528 \cdot 10^{-3} \mu A/cm²).

The decrease in current density decreases the intensity of the corrosion in composite specimens, which in turn reduces the rate of the corrosion. The polarization resistance (R_p) increases with increase in Gr content in Co-matrix composites, which also substantiate the reduction in corrosion rate of the Co-Gr nanocomposites.

3.6. Electrochemical Impedance Spectroscopy Analysis

The NY–Quist impedance for the Co–25Gr nanocomposite, which is identified as better corrosion composite by potentiometric polarization test, is obtained using electrochemical impedance spectroscopy (EIS). The electron transfer across the composite surface can be measured using charge transfer resistance R_{ct} , which is inversely proportional to corrosion rate.

Figure 9 shows the EIS spectra of Co-25Gr nanocomposites, which consist of two semicircles with smaller and larger circles at higher and lower frequency region.

The smaller circle depict the charge transfer resistance R_{ct1} at the interface of the counter electrode and NaCl solution and the bigger semicircle begin from the charge transfer resistance R_{ct2} of the smaller circle because of the electron transfer within the Co-Gr nanocomposite and charge transfer at the interface of Co-Gr and NaCl solution.

From the results, it is clear that the Co-25Gr nanocomposite has better corrosion resistance as a result of an increase in charge transfer resistance and a decrease in double layer capacitance. The results of EIS are showed in Table 2.



Fig. 9. EIS spectra of Co-25Gr nanocomposites.

TABLE 2. Charge transfer resistance obtained from EIS data fitting by equivalent circuit model.

Specimen	c_{dl1} , F	R_{ct1} , Ω	$m{c}_{dl2}, \mathbf{F}$	R_{ct2} , Ω
Co-25Gr	0.00247	20.08	0.000247	100

3.7. Immersion Test Analysis

The weight loss method is employed to study the percentage of weight loss of the composite materials in acidic and brine solutions such as HCl, H_2SO_4 and NaCl solutions. The composites are immersed in the different normality of above-said solutions for 24 hours. After remov-



Fig. 10. Graphical representation of weight loss in different media.

	% of weight loss						
Specimen	HCl		$\mathrm{H_2SO}_4$		NaCl		
	0.1 N	0.5 N	0.1 N	0.5 N	5%	10%	
Co-25Gr	0.78	2.01	2	4.04	0.14	0.25	
Co-20Gr	0.99	2.5	4.2	6.15	0.16	0.29	
Co-15Gr	1.05	3.2	6.3	8.11	0.19	0.34	
Co-10Gr	1.16	3.9	8.7	12.12	0.26	0.42	
Co-5Gr	1.19	4.2	10	14	0.36	0.59	
Pure Co	1.24	4.5	12	17	0.39	0.65	

TABLE 3. Percentage of weight loss in different media.

ing the specimen, it is washed and dried at room temperature. The weights of the specimens are noted before and after the immersion.

The percentage of weight loss is calculated by using the initial and final weight of the specimens. The percentage of weight loss is shown in Table 3 and the graphical representation is shown in Fig. 10.

4. CONCLUSIONS

The Co–Gr nanocomposites were prepared by employing high-energy ball mill and warm compacting process. The wear and corrosion resistance of the composites are studied in different conditions. The wear analysis on a pin on disc apparatus shows that Co–25Gr nanocomposite has better wear resistance and coefficient of friction.

The potentiometric polarization analysis shows that the Co-25Gr has improved corrosion resistance in various corrosive media, and the composites also show the signs of passivation due to the presence of Gr nanoparticles.

The EIS spectra also demonstrate the improvement in corrosion rate, which was due to the increase in charge transfer resistance of the composite material.

The immersion test also reveals that the Co-25Gr nanocomposite has improved corrosion resistance than pure Co. From the findings of this study, it can be concluded that the Co-25Gr nanocomposite has better wear and corrosion resistance.

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REFERENCES

- 1. L. M. Vilhena, C. M. Fernandes, E. Soares, J. Sacramento, A. M. R. Senos, and A. Ramalho, *Wear*, **346**–**347**: 99 (2016).
- Y. Liu, J. Cheng, B. Yin, S. Zhu, Z. Qiao, and J. Yang, *Tribol. Int.*, 109: 19 (2016).
- 3. F. Ren, W. Zhu, and K. Chu, J. Mech. Behav. Biomed. Mater., 68: 115 (2017).
- 4. R. Mousavi, M. E. Bahrololoom, and F. Deflorian, *Mater. Design*, **110**: 456 (2016).
- 5. R. Liu, J. Yao, Q. Zhang, M. X. Yao, and R. Collier, *Mater. Design*, 78: 95 (2015).
- 6. C. Jiang, Y. Xing, F. Zhang, and J. Hao, *Int. J. Miner. Metall. Mater.*, 19, Iss. 7: 657 (2012).

- 7. M. M. H. Bastwros, A. M. K. Esawi, and A. Wifi, *Wear*, **307**, Iss. 1–2:164 (2013).
- 8. K. S. Prakash, P. Balasundar, S. Nagaraja, P. M. Gopal and V. Kavimani, *J. Magnesium Alloys*, 4, Iss. 3: 197 (2016).
- P. Wang, H. Zhang, J. Yin, X. Xiong, C. Tan, C. Deng and Z. Yan, *Wear*, 380–381: 59 (2017).
- 10. T. R. Prabhu, V. K. Varma, and S. Vedantam, *Wear*, 309, Iss. 1–2: 247 (2014).
- C. Parswajinan, B.V. Ramnath, C. Elanchezhian, S. V. Pragadeesh, P. R. Ramkishore, and V. Sabarish, *Procedia*. *Eng.*, 97: 513 (2014).
- 12. Mohammad Sharear kabir, Tamzid lbn Minhaj, Md Delower Hossain, and ASW Kurny, *Am. J. Mater. Eng. Technol.*, 3, Iss. 1: 7 (2015).
- 13. C. Y. H. Lim, D. K. Leo, J. J. S. Ang, and M. Gupta, *Wear*, **259**, Iss. 1–6: 620 (2005).
- 14. F. Toptan, A. C. Alves, I. Kerti, E. Ariza, and L. A. Rocha, *Wear*, **306**, Iss. 1–2: 27 (2013).
- 15. N. Elkhoshkhany, A. Hafnway, and A. Khaled, *J. Alloys Compd.*, **695**: 1505 (2017).
- 16. F. A. P. Fernandes, J. Gallego, C. A. Picon, G. T. Filho, and L. C. Casteletti, *Surf. Coat. Technol.*, **279**: 112 (2015).
- 17. J. H. Qiu and P. H. Chua, Surf. Interface Anal., 28: 119 (1999).
- 18. T. S. N. Sankara Narayanan, I. Baskaran, K. Krishnaveni, and S. Parthiban, *Surf. Coat. Technol.*, **200**, Iss. 11: 3438 (2006).
- 19. Q. Xu, K. Gao, Y. Wang, and X. Pang, Appl. Surf. Sci., 345: 10 (2015).