

Estimating the Generalized Exponential Distribution Parameters and the Acceleration Factor under Constant-Stress Partially Accelerated Life Testing with Type-II Censoring

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Оценка параметров обобщенного экспоненциального распределения и коэффициента ускорения в условиях частично ускоренного ресурсного испытания с постоянным напряжением при цензурировании типа II

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Ускоренные и частично ускоренные ресурсные испытания часто проводятся для обеспечения надежности современной техники. Цель таких испытаний – короткий срок и с меньшими затратами получить информацию о ресурсе изделий и материалов. Испытания можно проводить при постоянных, ступенчатых, прогрессирующих и циклических нагрузках, а также при нагрузке случайным напряжением. Рассматривается задача оценки параметров обобщенного экспоненциального распределения и коэффициента ускорения в условиях частично ускоренного ресурсного испытания с постоянным напряжением. С использованием среднеквадратической погрешности проведено численное исследование эффективности оценки методом максимального правдоподобия для разных размеров образцов и значений параметра. Для параметров модели построены приблизительные доверительные границы. Чтобы получить доверительные границы для параметров модели в случае образца маленького размера, использовали метод отношения правдоподобия. В качестве примера проведено исследование с помощью моделирования. Показано, что результаты моделирования согласуются с данными расчетов.

Ключевые слова: техника обеспечения надежности, частично ускоренные ресурсные испытания, постоянное напряжение, обобщенное экспоненциальное распределение, оценка по методу максимального правдоподобия, границы отношения правдоподобия, цензурирование типа II.

Notation

ALT	– accelerated life testing
PALT	– partially accelerated life testing
CSPALT	– constant-stress partially accelerated life testing
GE	– generalized exponential
MTTF	– mean time to failure
ML	– maximum likelihood

<i>MLEs</i>	– maximum likelihood estimates/estimators
<i>LR</i>	– likelihood ratio
<i>LRB</i>	– likelihood ratio bounds
<i>MSE</i>	– mean square error
<i>CI</i>	– confidence interval
$1-\gamma$	– confidence level
IW_{95}	– <i>CI</i> width at 95% level of confidence
IW_{99}	– <i>CI</i> width at 99% level of confidence
n	– total number of test items in a <i>PALT</i> (sample size)
$y_{(r)}$	– the time of the r th failure at which the test is terminated
X	– lifetime of an item at normal (use) condition
Y	– lifetime of an item at accelerated condition
(\cdot)	– denotes maximum likelihood estimate
β	– acceleration factor ($\beta > 1$)
α	– GE shape parameter ($\alpha > 0$)
λ	– GE scale parameter ($\lambda > 0$)
x_i	– observed lifetime of item i tested at use condition
y_j	– observed lifetime of item j tested at accelerated condition
δ_{ui}, δ_{aj}	– indicator functions: $\delta_{ui} \equiv I(X_i \leq y_{(r)})$, $\delta_{aj} \equiv I(Y_j \leq y_{(r)})$, $i = 1, \dots, n$
π	– proportion of sample units allocated to accelerated condition
n_u, n_a	– numbers of items failed at use and accelerated conditions, respectively
r	– total number of failed units ($r = n_u + n_a$)
$L_{ui}(x_i, \delta_{ui})$	– the likelihood for (x_i, δ_{ui}) , $i = 1, \dots, n_u$
$L_{aj}(y_j, \delta_{aj})$	– the likelihood for (y_j, δ_{aj}) , $j = 1, \dots, n_a$
$x_{(1)} \leq \dots \leq x_{(n_u)} \leq y_{(r)}$	– ordered failure times at use condition
$y_{(1)} \leq \dots \leq y_{(n_a)} \leq y_{(r)}$	– ordered failure times at accelerated condition

Introduction. Accelerated life testing (ALT) is frequently used in modern reliability engineering. By performing life tests at accelerated (i.e., harsher-than-use) conditions, failures are quickly obtained, and products' reliability at normal (use) conditions can then be estimated via a stress-life relationship (data-extrapolation). In some cases such relationship is not known or can't be assumed and then the ALT methods can't be applied. Alternatively, another test method namely partially accelerated life testing (PALT) can be used to estimate and analyze products' reliability.

Such PALT results in shorter lives than would be observed under use condition. In PALT some of test units can be run under use condition and the others under accelerated condition. (In ALT, test units are run only at accelerated condition. Interested readers can refer to Nelson [1] and Meeker and Escobar [2] which are two comprehensible sources for ALT).

As Nelson [1] indicates, the stress can be applied in various ways, commonly used methods are step-stress and constant-stress. Under step-stress PALT, a test

item is first run at use condition and, if it does not fail for a specified time, then it is run at accelerated condition until failure occurs or the observation is censored. But the constant-stress PALT runs each item at either use condition or accelerated condition only, i.e., each unit is run at a constant-stress level until the test is terminated. Accelerated test stresses involve higher than usual temperature, voltage, pressure, load, humidity, etc., or some combination of them. The objective of a PALT is then to collect more failure data in a limited time without necessarily using high stresses to all test units.

Compared with the step-stress accelerated life test (step-test), the constant-stress accelerated life test (constant-test) has some merits as follows: simple test method, ripe theory, and precise test data. The constant-stress accelerated-life-test is commonly used to test the reliability of electric appliances. For an overview of constant-stress PALT (CSPALT), there are few studies in the literature in this respect: Bai and Chung [3] used the maximum likelihood method to estimate the scale parameter and the acceleration factor for exponentially distributed lifetimes under type-I censoring. Abdel-Ghani [4] considered the estimation problem for the Weibull distribution parameters. Ismail [5] used the maximum likelihood approach for estimating the acceleration factor and the parameters of Pareto distribution of the second kind. Ismail [6] extended the work of Abdel-Ghani [4] to study the problem of optimal design of the life test with type-II censored data. Recently, Ismail et al. [7] developed optimum constant-stress life test plans for Pareto distribution under type-I censoring.

The objective of this paper is to consider the CSPALT with type-II censoring for estimating the acceleration factor and the generalized exponential distribution parameters. A new distribution named as generalized exponential (GE) distribution or exponentiated exponential distribution was introduced by Gupta and Kundu [8] and since then it received a considerable attention in the literature. Several properties of the GE distribution were studied quite extensively; see for example, Gupta and Kundu [8–11]. The readers may be referred to some of the related literature on GE distribution by Raqab [12], Raqab and Ahsanullah [13] and Zheng [14]. The simple mathematical structure of the GE distribution enables it to be used effectively for modeling various lifetime data types with possible censoring or grouping Baklizi [15].

The two-parameter GE family has the distribution function

$$F(x; \alpha, \lambda) = (1 - e^{-\lambda x})^\alpha, \quad y > 0. \quad (1)$$

The corresponding density function is

$$f_X(x; \alpha, \lambda) = \alpha \lambda (1 - e^{-\lambda x})^{\alpha-1} e^{-\lambda x}, \quad x > 0, \quad \alpha > 0, \quad \lambda > 0, \quad (2)$$

where α and λ are the shape and scale parameters, respectively. When $\alpha=1$ it coincides with the exponential distribution with mean $1/\lambda$. When $\alpha \leq 1$ the density function is strictly decreasing and for $\alpha > 1$ it has a unimodal shape. These densities are illustrated in Gupta and Kundu [9]. It is clear that the GE density functions are always right skewed and it is observed that GE distributions can be used quite effectively to analyze skewed data sets.

The hazard rate function of the GE distribution is

$$h(x; \alpha, \lambda) = \frac{\alpha \lambda e^{-\lambda x} (1 - e^{-\lambda x})^{\alpha-1}}{1 - (1 - e^{-\lambda x})^\alpha}, \quad (3)$$

and the *MTTF* is

$$MTTF = \sum_{i=1}^{\infty} \binom{\alpha}{i} \frac{(-1)^{i+1}}{i\lambda}. \quad (4)$$

The GE distribution can have increasing and decreasing hazard rates depending on the shape parameter α . The hazard rate increases from 0 to λ if $\alpha > 1$ and if $\alpha < 1$ it decreases from ∞ to λ . This property leads to a good ability of using this distribution in reliability and life testing, Abuammoh and Sarhan [16].

The remainder of the paper is organized as follows: in Section 1 the test procedure and its assumptions used throughout this paper are presented. In Section 2 two different methods are used to obtain the estimations of the unknown parameters. The first method is the maximum likelihood (ML) method when the sample size is large and the second one is the likelihood ratio bounds (LRB) method when the sample size is small. In Section 3 simulation studies are carried out to illustrate the theoretical results.

1. Test Procedure and Its Assumption. The test procedure of the CSPALT and its assumptions are described as follows:

Test Procedure. In a CSPALT, the total sample size n of test units is divided into two parts such that:

1. $n\pi$ units randomly chosen among n test units sampled are allocated to accelerated condition and the remaining are allocated to use condition.

2. Each test unit is run until it fails or the test is terminated.

Assumptions.

1. The lifetimes X_i , $i = 1, \dots, n(1 - \pi)$ of units allocated to use condition, are i.i.d. r.v.'s.

2. The lifetimes Y_j , $j = 1, \dots, n\pi$ of units allocated to accelerated condition, are i.i.d r.v.'s.

3. The lifetimes X_i and Y_j are mutually statistically-independent.

4. The lifetimes of the test units follow the GE distribution.

2. Parameter Estimation.

2.1. ML Estimation. In a simple constant-stress PALT, the test item is run either at use condition or at accelerated condition only. Since the lifetimes of the test items follow the GE distribution, the probability density function (pdf) of an item tested at use condition is given as in (2). While for an item tested at accelerated condition, the pdf is given by

$$f_Y(y; \beta, \alpha, \lambda) = \beta \alpha \lambda (1 - e^{-\beta \lambda y})^{\alpha-1} e^{-\beta \lambda y}, \quad (5)$$

$$y > 0, \quad \beta > 1, \quad \alpha > 0, \quad \lambda > 0,$$

where $Y = \beta^{-1} X$.

Since the test in type-II censoring is terminated at a predetermined r of failures, the observed lifetimes $x_{(1)} \leq \dots \leq x_{(n_u)} \leq y_{(r)}$ and $y_{(1)} \leq \dots \leq y_{(n_a)} \leq y_{(r)}$ are ordered failure times at use and accelerated conditions respectively, where n_u and n_a are the numbers of items failed at use and accelerated conditions, respectively.

Let the indicator functions: $\delta_{ui} \equiv I(X_i \leq y_{(r)})$ and $\delta_{aj} \equiv I(Y_j \leq y_{(r)})$. Then the total likelihood for $(x_1; \delta_{u1}, \dots, x_{n(1-\pi)}; \delta_{un(1-\pi)}, y_1; \delta_{a1}, \dots, y_{n\pi}; \delta_{an\pi})$ is given by

$$\begin{aligned} L(\underline{x}, \underline{y} | \beta, \alpha, \lambda) &\propto \prod_{i=1}^{n\bar{\pi}} L_{ui}(x_i, \delta_{ui} | \alpha, \lambda) \prod_{j=1}^{n\pi} L_{aj}(y_j, \delta_{aj} | \beta, \alpha, \lambda) = \\ &= \prod_{i=1}^{n\bar{\pi}} \{\alpha \lambda (1 - e^{-\lambda_{x_i}})^{\alpha-1} e^{-\lambda_{x_i}}\}^{\delta_{ui}} \{1 - (1 - e^{-\lambda_{y_{(r)}}})^\alpha\}^{\bar{\delta}_{ui}} \times \\ &\quad \times \prod_{j=1}^{n\pi} \{\beta \alpha \lambda (1 - e^{-\beta \lambda_{y_j}})^{\alpha-1} e^{-\beta \lambda_{y_j}}\}^{\delta_{aj}} \{1 - (1 - e^{-\beta \lambda_{y_{(r)}}})^\alpha\}^{\bar{\delta}_{aj}}, \end{aligned} \quad (6)$$

where

$$\bar{\delta}_{ui} = 1 - \delta_{ui}, \quad \bar{\delta}_{aj} = 1 - \delta_{aj}, \quad \text{and} \quad \bar{\pi} = 1 - \pi.$$

We can write the total likelihood function by another possibility, in terms of the order statistics indicated earlier, as

$$\begin{aligned} L(\underline{x}, \underline{y} | \beta, \alpha, \lambda) &\propto \prod_{i=1}^{n_u} \{\alpha \lambda (1 - e^{-\lambda_{x_i}})^{\alpha-1} e^{-\lambda_{x_i}}\} \prod_{i=n_u+1}^{n\bar{\pi}} \{1 - (1 - e^{-\lambda_{y_{(r)}}})^\alpha\} \times \\ &\quad \times \prod_{j=1}^{n_a} \{\beta \alpha \lambda (1 - e^{-\beta \lambda_{y_j}})^{\alpha-1} e^{-\beta \lambda_{y_j}}\} \prod_{j=n_a+1}^{n\pi} \{1 - (1 - e^{-\beta \lambda_{y_{(r)}}})^\alpha\}. \end{aligned}$$

The log-likelihood function, $\ln L$, is

$$\begin{aligned} \ln L &= n_u \ln \alpha + n_u \ln \lambda + (\alpha - 1) \sum_{i=1}^{n\bar{\pi}} \ln(1 - e^{-\lambda_{x_i}}) - \lambda \sum_{j=1}^{n\pi} x_i + \\ &\quad + n_u \ln[1 - (1 - e^{-\lambda_{y_{(r)}}})^\alpha] + n_a \ln \beta + n_a \ln \alpha + n_a \ln(\lambda) + \\ &\quad + (\alpha - 1) \sum_{j=1}^{n\pi} \ln(1 - e^{-\beta \lambda_{y_j}}) - \beta \lambda \sum_{j=1}^{n\pi} y_j + n_a \ln[1 - (1 - e^{-\beta \lambda_{y_{(r)}}})^\alpha]. \end{aligned} \quad (7)$$

The normal equations become

$$\begin{aligned} \frac{\partial \ln L}{\partial \beta} = & \frac{n_a}{\beta} + (\alpha - 1)\lambda \sum_{i=1}^{n_a} \frac{y_j e^{-\beta \lambda y_j}}{1 - e^{-\beta \lambda y_j}} - \lambda \sum_{j=1}^{n_u} y_j - \\ & - \frac{\alpha \lambda y_{(r)} n_a e^{-\beta \lambda y_{(r)}} (1 - e^{-\beta \lambda y_{(r)}})^{\alpha-1}}{1 - (1 - e^{-\beta \lambda y_{(r)}})^\alpha} = 0, \end{aligned} \quad (8)$$

$$\begin{aligned} \frac{\partial \ln L}{\partial \alpha} = & \frac{n_u + n_a}{\alpha} + \sum_{i=1}^{n_u} \ln(1 - e^{-\lambda x_i}) + \sum_{j=1}^{n_a} \ln(1 - e^{-\beta \lambda y_j}) - \\ & - \frac{n_u (1 - e^{-\lambda y_{(r)}})^\alpha \ln(1 - e^{-\lambda y_{(r)}})}{1 - (1 - e^{-\lambda y_{(r)}})^\alpha} - \frac{n_a (1 - e^{-\beta \lambda y_{(r)}})^\alpha \ln(1 - e^{-\beta \lambda y_{(r)}})}{1 - (1 - e^{-\beta \lambda y_{(r)}})^\alpha} = 0, \end{aligned} \quad (9)$$

$$\begin{aligned} \frac{\partial \ln L}{\partial \lambda} = & \frac{n_u + n_a}{\lambda} + (\alpha - 1) \sum_{i=1}^{n_u} \frac{x_i e^{-\lambda x_i}}{(1 - e^{-\lambda x_i})} - \\ & - \sum_{j=1}^{n_u} x_i - \frac{n_u \alpha y_{(r)} (1 - e^{-\lambda y_{(r)}})^{\alpha-1} e^{-\lambda y_{(r)}}}{1 - (1 - e^{-\lambda y_{(r)}})^\alpha} + (\alpha - 1) \beta \sum_{i=1}^{n_a} \frac{y_j e^{-\beta \lambda y_j}}{(1 - e^{-\beta \lambda y_j})} - \\ & - \beta \sum_{j=1}^{n_a} y_j - \frac{n_a \alpha \beta y_{(r)} (1 - e^{-\beta \lambda y_{(r)}})^{\alpha-1} e^{-\beta \lambda y_{(r)}}}{1 - (1 - e^{-\beta \lambda y_{(r)}})^\alpha} = 0. \end{aligned} \quad (10)$$

Now, we have a system of three nonlinear equations in three unknowns β , α , and λ . It is clear that a closed form solution is very difficult to obtain. Therefore, iterative procedure can be used to find a numerical solution of the above system.

Concerning the asymptotic confidence intervals of the model parameters, it is not possible to derive the exact distributions of the *MLE* of the parameters because the likelihood equations have no closed form solutions in the unknown parameters β , α , and λ . Thus, approximate confidence intervals of the parameters are derived based on the asymptotic distributions of the *MLE* of the elements of the vector of unknown parameters $\theta = (\beta, \alpha, \lambda)$. It is known that the asymptotic distribution of the *MLE* of θ is given by (see Miller [17])

$$((\hat{\beta} - \beta), (\hat{\alpha} - \alpha), (\hat{\lambda} - \lambda)) \rightarrow N(0, I^{-1}(\beta, \alpha, \lambda)),$$

where $I^{-1}(\beta, \alpha, \lambda)$ is the variance-covariance matrix of the unknown parameters $\theta = (\beta, \alpha, \lambda)$. The elements of the 3×3 matrix I , $I_{ij}(\beta, \alpha, \lambda)$, $i, j = 1, 2, 3$; can be approximated by $I_{ij}(\hat{\beta}, \hat{\alpha}, \hat{\lambda})$, where

$$I_{ij}(\hat{\theta}) = -\frac{\partial^2 \ln L(\theta)}{\partial \theta_i \partial \theta_j} \Big|_{\theta=\hat{\theta}}.$$

From Eq. (7), we get the following:

$$\begin{aligned} \frac{\partial^2 \ln L}{\partial \beta^2} &= -\frac{n_a}{\beta^2} - (\alpha - 1)\lambda^2 \sum_{j=1}^{n_a} \frac{y_j^2 e^{-\beta \lambda_{y_j}} \psi_{3j} + y_j^2 e^{-2\beta \lambda_{y_j}}}{\psi_{3j}^2} - \\ &- \frac{\alpha \lambda^2 y_{(r)}^2 e^{-\beta \lambda_{y(r)}} n_a \{[(\alpha - 1)\psi_5 e^{-\beta \lambda_{y(r)}} - \psi_5^2][1 - \psi_5^\alpha] + \alpha \psi_5^{2(\alpha-1)} e^{-\beta \lambda_{y(r)}}\}}{\psi_5^2}, \quad (11) \end{aligned}$$

$$\begin{aligned} \frac{\partial^2 \ln L}{\partial \alpha^2} &= -\frac{n_u}{\alpha^2} - \frac{n_u \psi_2^\alpha (\ln \psi_2)^2 \{(1 - \psi_2^\alpha) + \psi_2^\alpha\}}{(1 - \psi_2^\alpha)^2} - \frac{n_a}{\alpha^2} - \\ &- \frac{n_a (\ln \psi_6)^2 \{\psi_5 \psi_6^\alpha + (1 - \psi_5)^2\}}{\psi_5^2}, \quad (12) \end{aligned}$$

$$\begin{aligned} \frac{\partial^2 \ln L}{\partial \lambda^2} &= -\frac{n_u + n_a}{\lambda^2} - (\alpha - 1) \sum_{i=1}^{n_u} \frac{x_i^2 e^{-\lambda_{x_i}} (\psi_{1i} + e^{-\lambda_{x_i}})}{\psi_{1i}^2} - \\ &- \frac{n_u \alpha y_{(r)}^2 \{[(\alpha - 1)\psi_2^{\alpha-2} e^{-\lambda_{y(r)}} - \psi_2^{\alpha-1} e^{-\lambda_{y(r)}}][1 - \psi_2^\alpha] + \alpha \psi_2^{2(\alpha-1)} e^{-2\lambda_{y(r)}}\}}{\psi_5^2} + \\ &+ (\alpha - 1)\beta^2 \sum_{j=1}^{n_a} \frac{y_j^2 e^{-\beta \lambda_{y_j}} (\psi_{3j} - e^{-\beta \lambda_{y_j}})}{\psi_{3j}^2} - \\ &- \frac{n_a \alpha \beta^2 y_{(r)}^2 \{\psi_5 e^{-\beta \lambda_{y(r)}} [(\alpha - 1)\psi_6^{\alpha-2} - \psi_6^{\alpha-1}] + \alpha \psi_6^{2(\alpha-1)} e^{-2\beta \lambda_{y(r)}}\}}{\psi_5^2}, \quad (13) \end{aligned}$$

$$\begin{aligned} \frac{\partial^2 \ln L}{\partial \beta \partial \alpha} &= \lambda \sum_{j=1}^{n_a} \frac{y_j e^{-\beta \lambda_{y_j}}}{\psi_{3j}} - \\ &- \frac{n_a \lambda y_{(r)} e^{-\beta \lambda_{y(r)}} \{[\psi_6^{\alpha-2} + \alpha \psi_6^{\alpha-1} \ln \psi_6] \psi_5 + \alpha \psi_6^{2(\alpha-1)} \ln \psi_6\}}{\psi_5^2}, \quad (14) \end{aligned}$$

$$\frac{\partial^2 \ln L}{\partial \beta \partial \lambda} = (\alpha - 1) \left\{ \sum_{j=1}^{n_a} \frac{y_j e^{-\beta \lambda_{y_j}}}{\psi_{3j}} - \lambda \beta \sum_{j=1}^{n_a} \frac{y_j^2 e^{-\beta \lambda_{y_j}} (\psi_{3j} + e^{-\beta \lambda_{y_j}})}{\psi_{3j}^2} \right\} - \sum_{j=1}^{n_a} y_j -$$

$$\begin{aligned}
& - \frac{n_a \alpha y_{(r)} e^{-\beta \lambda y_{(r)}}}{\psi_5^2} \{ [1 - \lambda \beta y_{(r)} \psi_6^{\alpha-1} + (\alpha-1) \lambda \beta y_{(r)} e^{-\beta \lambda y_{(r)}} \psi_6^{\alpha-2}] \psi_5 + \\
& + \alpha \lambda e^{-\beta \lambda y_{(r)}} \psi_6^{2(\alpha-1)} \}, \tag{15}
\end{aligned}$$

$$\begin{aligned}
\frac{\partial^2 \ln L}{\partial \alpha \partial \lambda} = & \sum_{i=1}^{n_u} \frac{x_i e^{-\lambda x_i}}{\psi_{1i}} + \beta \sum_{j=1}^{n_a} \frac{y_j e^{-\beta \lambda y_j}}{\psi_{3j}} - \\
& - \frac{n_u}{\psi_4^2} \{ [\alpha y_{(r)} \psi_2^{\alpha-1} e^{-\lambda y_{(r)}} - \ln \psi_2] + y_{(r)} \psi_2^{\alpha-1} e^{-\lambda y_{(r)}} \} \psi_4 + \\
& + \alpha y_{(r)} \psi_2^{2\alpha-1} \ln \psi_2 e^{-\lambda y_{(r)}} \} - \frac{n_a}{\psi_5^2} \{ [\alpha y_{(r)} \beta \psi_6^{\alpha-1} e^{-\beta \lambda y_{(r)}} \ln \psi_6 + \\
& + y_{(r)} \beta \psi_6^{\alpha-1} e^{-\beta \lambda y_{(r)}}] \psi_5 + \alpha y_{(r)} \beta \psi_6^{2\alpha-1} \ln \psi_6 e^{-\beta \lambda y_{(r)}} \}, \tag{16}
\end{aligned}$$

where

$$\begin{aligned}
\psi_{1i} &= 1 - e^{-\lambda x_i}, \quad \psi_2 = 1 - e^{-\lambda y_{(r)}}, \quad \psi_{3j} = 1 - e^{-\beta \lambda y_j}, \\
\psi_4 &= 1 - (1 - e^{-\lambda y_{(r)}})^\alpha, \quad \psi_5 = 1 - (1 - e^{-\beta \lambda y_{(r)}})^\alpha, \quad \psi_6 = 1 - e^{-\beta \lambda y_{(r)}}.
\end{aligned}$$

Thus, the approximate $100(1-\gamma)\%$ two sided confidence intervals for β , α , and λ are, respectively, given by

$$\hat{\beta} \pm Z_{\gamma/2} \sqrt{I_{11}^{-1}(\hat{\beta})}, \quad \hat{\alpha} \pm Z_{\gamma/2} \sqrt{I_{22}^{-1}(\hat{\alpha})}, \quad \hat{\lambda} \pm Z_{\gamma/2} \sqrt{I_{33}^{-1}(\hat{\lambda})},$$

where $Z_{\gamma/2}$ is the upper $100(\gamma/2)$ th percentile of a standard normal distribution.

2.2. LRB Estimation. The ML estimates are based on large sample normal theory. However, when there are only few failures, the large sample normal theory is not very accurate. Thus, the ML estimates could be very different from the true values. The LRB method is based on the χ^2 -squared distribution assumption. For example, Vander Wiel and Meeker [18] investigated the accuracy of the likelihood ratio (LR)-based confidence bounds and asymptotic s-normal-based confidence bounds using censored Weibull regression data from constant-stress ALT. It is noted that the LR bounds perform better than the ML-based bounds when the sample size is small. In this subsection we will use the LRB method to obtain the confidence bounds of the model parameters when the sample size is small.

Here, we will apply the LRB method to derive the confidence bounds for a vector of unknown parameters $\theta(\beta, \alpha, \lambda)$ when the sample size is small. We treat the LR as a function on θ defined by

$$LR(\theta) = \frac{L(\beta, \alpha, \lambda)}{L(\hat{\beta}, \hat{\alpha}, \hat{\lambda})},$$

where $L(\beta, \alpha, \lambda)$ is the likelihood function with three parameters β , α , and λ , and $\hat{\beta}$, $\hat{\alpha}$, and $\hat{\lambda}$ are their estimated values.

Because the log likelihood ratio statistic is X^2 distributed, that is, $-2\log LR(\theta) \approx X_{\gamma,k}^2$, with k degrees of freedom (the number of quantities jointly estimated), then, the confidence bounds over which $LR(\theta) > e^{X_{\gamma,k}^2/2}$ is the $100(1-\gamma)\%$ LRB for θ .

There is no closed-form solution available. Therefore, it is very difficult (there are more than two parameters) to discuss LR bounds except for simulation study which has been done by others (e.g., McSorley et al. [19]). The simulation results of the LR bounds of our model parameters are presented in Tables 1 and 2. For the LR bounds of the model parameters when the sample size is small, the simulation results are calculated based on the χ^2 -squared distribution and are reported in these tables. These results support the theoretical findings.

Table 1

Simulation Results of the LR Bounds of the Model Parameters Using Small Samples
($\beta = 1.3$, $\alpha = 0.5$, and $\lambda = 0.7$)

n	Parameter	Lower bound	Upper bound	Lower bound	Upper bound
		95%	95%	99%	99%
10	β	0.88330	2.363765	0.794970	2.659236
	α	0.33932	0.673620	0.305388	0.757823
	λ	0.36953	0.948625	0.332577	1.067203
15	β	0.81750	2.199545	0.735750	2.474488
	α	0.37065	0.650370	0.333585	0.731666
	λ	0.24325	0.743185	0.218925	0.836083
20	β	0.93918	1.870935	0.845262	2.104802
	α	0.42480	0.632850	0.382320	0.711956
	λ	0.42942	0.813705	0.386478	0.915418
25	β	0.99072	1.641350	0.891648	1.846519
	α	0.45559	0.623440	0.410031	0.701370
	λ	0.48816	0.802060	0.439344	0.902318

3. Simulation Studies. In this section, a simulation study is conducted to illustrate the theoretical results given in this paper and to investigate the performance of the MLEs of the model parameters via their mean square error (MSE). Moreover, the performance of the various approximate intervals presented in this paper is studied. The simulation algorithm or procedure can be described as follows.

Step 1. 10,000 random samples of sizes 30, 50, 75, and 100 are generated from the GE distribution. Two sets of the true parameter values β , α , and λ are considered to be 1.3, 0.5, 0.7 and 2.2, 1.4, 1.1, respectively.

Step 2. Considering the allocation parameter π to be $\pi = 0.5$.

Step 3. For the two sets of parameters and for each sample size, the two parameters of the GE distribution and the acceleration factor are estimated under CSPALT with type-II censored data using the maximum likelihood approach.

Table 2

Simulation Results of the LR Bounds of the Model Parameters Using Small Samples
 $(\beta = 2.2, \alpha = 1.4, \text{ and } \lambda = 1.1)$

n	Parameter	Lower bound 95%	Upper bound 95%	Lower bound 99%	Upper bound 99%
10	β	1.44683	5.771750	1.229806	6.060338
	α	0.70889	2.826875	0.602557	2.968219
	λ	0.16919	1.813125	0.143812	1.903781
15	β	1.51844	4.416750	1.290674	4.637588
	α	0.75075	2.357875	0.638138	2.475769
	λ	0.35182	1.674500	0.299047	1.758225
20	β	1.67937	3.528875	1.127465	3.705319
	α	0.92281	1.810375	0.784389	1.900894
	λ	0.71729	1.558125	0.609697	1.636031
25	β	1.72627	3.322625	1.267330	3.488756
	α	0.86569	1.615125	0.735837	1.695881
	λ	0.84035	1.549625	0.714298	1.627106

Table 3

Average Values of the MLEs, MSE, Variance, IW_{95} , and IW_{99}
 $(\beta = 1.3, \alpha = 0.5, \text{ and } \lambda = 0.7)$

n	Parameter	MLE	MSE	Variance	IW_{95}	IW_{99}
30	β	1.193727	0.326016	0.132593	1.427402	1.878927
	α	0.757161	0.231624	0.004154	0.252650	0.332570
	λ	0.528947	0.104616	0.010251	0.396889	0.522436
50	β	1.233921	0.175032	0.132593	1.266506	1.667135
	α	0.664767	0.141264	0.004154	0.210406	0.276963
	λ	0.590717	0.070704	0.010251	0.276019	0.363331
75	β	1.272472	0.114624	0.008442	0.360171	0.474103
	α	0.568719	0.081504	0.001742	0.163610	0.215364
	λ	0.664158	0.035064	0.002948	0.212838	0.280165
100	β	1.318393	0.053496	0.001005	0.124271	0.163581
	α	0.501048	0.030888	0.000670	0.101467	0.133563
	λ	0.682955	0.062024	0.000871	0.115690	0.152286

Step 4. The Newton–Raphson method is used to solve the nonlinear likelihood equations for β , α , and λ numerically.

Step 5. The MSE of the $MLEs$ of model parameters is computed for different sized samples and different sets of parameter values.

Step 6. The asymptotic variances of the estimators of model parameters are estimated for different sized samples and different sets of parameter values.

Step 7. The approximate confidence bounds with confidence level $\gamma = 0.95$ and 0.99 are obtained for the three parameters of the model.

By conducting the above steps using a computer program written in the Pascal language, the simulation results are reported in Tables 3 and 4. As shown from the

Table 4

Average Values of the MLEs, MSE, Variance, IW_{95} , and IW_{99}
 $(\beta = 2.2, \alpha = 1.4, \text{ and } \lambda = 1.1)$

n	Parameter	MLE	MSE	Variance	IW_{95}	IW_{99}
30	β	3.412658	0.304116	0.106191	1.277409	1.681487
	α	0.919338	0.103726	0.089262	1.171168	1.541640
	λ	0.797132	0.171306	0.033372	0.716106	0.942629
50	β	2.905014	0.178002	0.061803	0.974520	1.282787
	α	1.083096	0.044950	0.048843	0.866338	1.140383
	λ	0.985296	0.082088	0.009639	0.384859	0.506601
75	β	2.303450	0.113274	0.021789	0.578635	0.761673
	α	1.321138	0.015686	0.026487	0.637973	0.839781
	λ	1.035468	0.037882	0.002835	0.208719	0.274743
100	β	2.225172	0.067518	0.001134	0.132006	0.173763
	α	1.394834	0.001744	0.000972	0.122214	0.160873
	λ	1.067906	0.009688	0.001458	0.149680	0.197028

numerical results, the maximum likelihood estimators have good statistical properties. The estimates of the parameters approach the true values as the sample size increases. Also, the estimated asymptotic variances of the estimators decrease as the sample size increases. Moreover, the estimated approximate confidence intervals for the three parameters are to be narrower when the sample size is getting to be larger.

Conclusions. In this paper the problem of estimating the generalized exponential distribution parameters and the acceleration factor in the case of constant-stress partially accelerated life tests was considered under type-II censoring. The maximum likelihood method was used to estimate the model parameters using the Newton–Raphson method. The performance of the estimators was investigated numerically for different parameter values and different sample sizes. Moreover, the approximate confidence bounds of the model parameters were obtained at 95 and 99% levels of confidence.

It is concluded that the numerical results support the theoretical findings. That is, the maximum likelihood estimators are consistent and their asymptotic variances decrease as the sample size increases. Moreover, the estimated approximate confidence intervals for the three parameters are to be smaller when the sample size is getting to be larger. In addition, the confidence intervals obtained at confidence level $\gamma = 0.95$ are narrower than those at $\gamma = 0.99$. Another method, namely, the LRB method was used to obtain the confidence bounds of the model parameters when the sample size is small. The simulation results of this method support the theoretical findings. That is, good estimations were obtained using this method when the sample size is small. As a future work, this study can be extended to deal with the problem of estimation using progressively type-II censored data assuming the same distribution under CSPALT.

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Резюме

Прискорені та частково прискорені ресурсні випробування часто проводяться для забезпечення надійності сучасної техніки. Метою таких випробувань є за короткий проміжок часу та з найменшими затратами отримати інформацію про ресурс виробів і матеріалів. Випробування можна проводити за постійних, східчастих, прогресуючих і циклічних навантажень, а також при навантаженні випадковим напруженням. Розглядається задача оцінки параметрів загального експоненціального розподілу та коефіцієнта прискорення в умовах частково прискореного ресурсного випробування з постійною напругою. Із використанням середньоквадратичної похибки проведено чисельне дослідження ефективності оцінки методом максимальної правдоподібності для різних розмірів зразка та значень параметра. Для параметрів моделі побудовано приблизні довірчі граници. Щоб отримати довірчі граници для параметра моделі у випадку зразка маленького розміру, використовували метод відношення правдоподібності. Як приклад проведено дослідження за допомогою моделювання. Показано, що результати моделювання збігаються з даними розрахунків.

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